



CYPRESS

Frequently Asked Questions about the RoboClock® Family

The following questions are frequently asked by customers who are using devices in the RoboClock® family. The RoboClock family consists of the RoboClock (CY7B991/2), RoboClock+ (CY7B9911), Low Voltage RoboClock (CY7B991V), Low Voltage RoboClock+ (CY7B9911V), and RoboClock Jr. (CY7B9910/20). These answers will serve as an introduction for each topic. It will be indicated when a separate application note covers the topics in more complete detail.

1. Can I use an external divider in my feedback loop?

Yes, it is possible to use external dividers in the feedback path. However, large dividers or dividers that have an inherently long delay, should be used cautiously. There are some constraints that should be followed. A large divider ratio can cause the phase detector update gaps to become excessively large. This will cause the VCO to drift excessively and result in output jitter. As a “rule of thumb” the maximum divider ratio in the feedback path should be less than 16. Larger values may be used with some consideration.

2. How do I achieve a 90-degree offset? How can I use an external divider to achieve a 90-degree offset independent of frequency?

The simplest way to achieve a 90-degree phase shift is to use the programmable skew functionality of RoboClock. An exact offset of 90 degrees is only available when the FS pin is in the HIGH state. When the FS pin is in the LOW or MID state, an offset close to 90 degrees is still attainable. The period of the VCO is divided into different amounts of time units (t_U) for each setting of the FS pin.

- $VCO_{period} = 44 t_U$ (FS=LOW)
- $VCO_{period} = 26 t_U$ (FS=MID)
- $VCO_{period} = 16 t_U$ (FS=HIGH)

A 90-degree offset is the $VCO_{period} / 4$. Therefore, a 90-degree offset would require an offset of:

- FS LOW = $\pm 11 t_U$ for a 90-degree offset
- FS MID = $\pm 6.5 t_U$ for a 90-degree offset
- FS HIGH = $\pm 4 t_U$ for a 90-degree offset

The offset of $\pm 4 t_U$ with FS = HIGH is achievable by simply programming the output to have a skew of $\pm 4 t_U$. However, it is not possible to get an exact offset of $\pm 11 t_U$ (FS=LOW) or $\pm 6.5 t_U$ (FS=MID). With FS in the MID position, an offset of $\pm 6 t_U$ or $\pm 7 t_U$ is possible. This creates a phase offset of ± 83 degrees ($\pm 6 t_U$) or ± 97 degrees ($\pm 7 t_U$). At 50 MHz a 90-degree phase shift is equal to ± 5 ns offset. The skewed outputs are shifted by ± 4.62 ns or ± 5.38 ns (off by ± 0.38 ns). With FS in the LOW position, an offset of ± 82 degrees ($\pm 10 t_U$) or ± 98 degrees ($\pm 12 t_U$) is possible. At 30 MHz, an exact 90-degree phase shift is equal to a ± 8.33 ns offset. The skewed outputs are shifted by ± 7.58 ns or ± 9.09 ns (off by ± 0.76 ns).

Offsets between outputs are achieved by selecting the appropriate skew taps as shown in *Table 1*. One of the specific outputs can be connected to FB. This establishes a zero phase reference, but the phase relationship between outputs is maintained even if another output (and skew) is used for FB.

Table 1. Skew Combinations for 90 Degree Offset

FS=HIGH	FS=MID	FS=HIGH
$\pm 4 t_U, 0 t_U$	$\pm 6 t_U, 0 t_U$	$\pm 6 t_U, \pm 6 t_U$
$\pm 6 t_U, \pm 2 t_U$	$\pm 2 t_U, \pm 4 t_U$	$\pm 6 t_U, \pm 4 t_U$
$\pm 2 t_U, \pm 2 t_U$	$\pm 3 t_U, \pm 3 t_U$	
$\pm 3 t_U, \pm 1 t_U$	$\pm 3 t_U, \pm 4 t_U$	
	$\pm 6 t_U, \pm 1 t_U$	

It is also possible to use external dividers, as *Figure 1* shows, to achieve a 90-degree offset independent of frequency. This example utilizes a negative-edge triggered D flip-flop as an external divider. It is possible to achieve a positive or negative

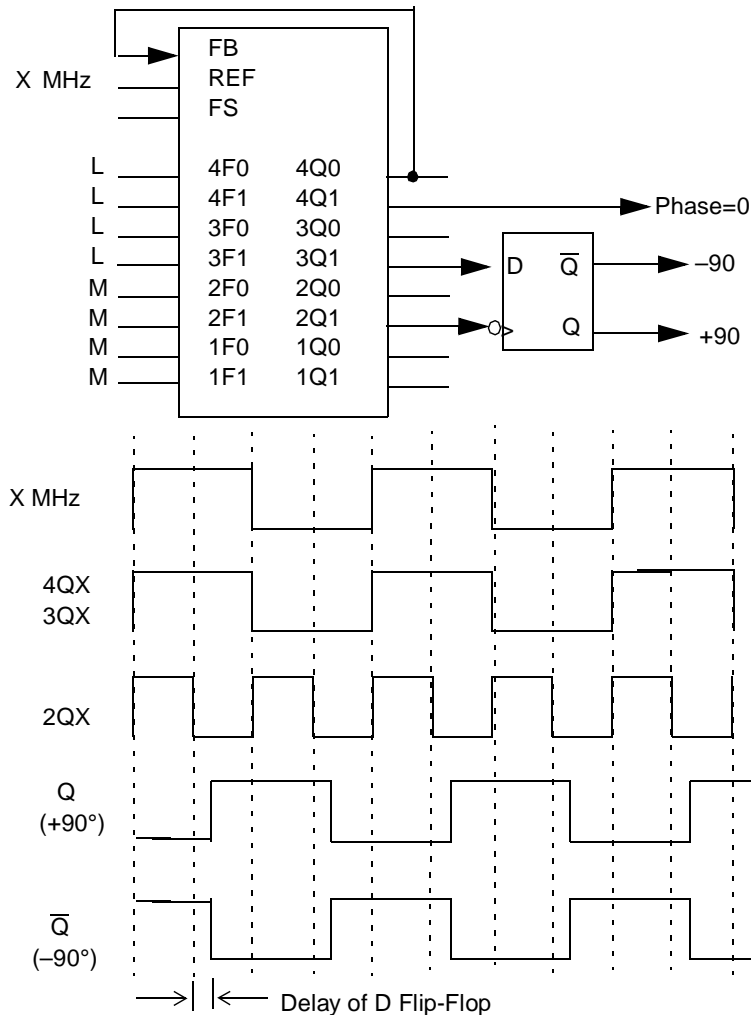


Figure 1. Circuit to Achieve a 90 Degree Offset

90-degree phase shift independent of the frequency range. The polarity of the phase is determined by choosing either the Q or \bar{Q} output from the D flip-flop. The delay of the D flip-flop can also be compensated by adjusting the programmable skew of the 2Q1 output of the RoboClock. It should be noted that the propagation delay of the D flip-flop is not typically controlled nor specified. Also, the Q and \bar{Q} delays may not be symmetrical. The compensating skew control of the RoboClock to account for the propagation delays may not hold over temperature, because most flip-flops exhibit significant variation while RoboClock does not.

3. What happens to the outputs when there is no REF input?

There are two scenarios that cause the output to react differently:

If REF is not connected during power-up, the behavior of the output will be probabilistic. The state is dependent upon internal circuitry that is controlled by the REF input. The output may be inactive (no output clock) or it may oscillate at the lowest possible frequency determined by the setting of the FS pin.

If the REF input is disconnected during steady state operation, the PLL will “think” that it is running too fast and will compensate by lowering the PLL frequency. The PLL frequency will be determined by the setting of the FS pin. The final frequency will be lower than the values stated in the data sheet. When the REF input is reconnected, the PLL will be out of phase and frequency alignment. It will compensate by increasing the PLL frequency and will overshoot the final frequency. It will continue in a damped oscillation state until the PLL “locks” onto the FB signal. This time is called t_{LOCK} in the data sheet.

4. Is RoboClock 3.3V-compatible?

The Low Voltage RoboClock (CY7B991V) and RoboClock+ (CY7B9911V) are completely 3.3V-compatible. The original RoboClock CY7B991/2 (along with the CY7B9910/20/11) requires a +5V V_{CC} supply. However, it is possible to make the output swing to 3.3V-compatible levels in the TTL RoboClock (CY7B991/10/11). The CMOS-level RoboClocks (CY7B992 and CY7B9920) cannot be made 3.3V-compatible due to their design, which produces rail-to-rail output swings.

Two termination networks are shown in Figure 2, either of which make RoboClock compatible with 3.3V systems. For a more in-depth explanation, an application note, "Using CY7B991 (RoboClock), CY7B9911 (RoboClock+) and CY7B9910 (Robo Jr.) in 3.3V Environments" is available from the Cypress Semiconductor Corporation website (<http://www.cypress.com>).

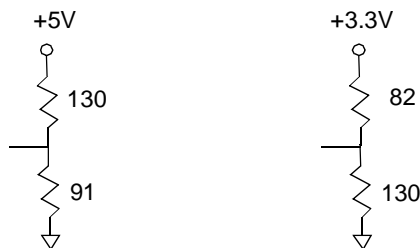


Figure 2. Typical 50Ω Termination to 5V and 3.3V for 3.3V-Compatible RoboClock Outputs

5. What are the jitter characteristics of RoboClock? Can you connect many RoboClocks in a cascaded configuration?

RoboClock is neither tolerant nor intolerant to jitter. It is more accurate to describe the jitter characteristics of RoboClock. The jitter transfer characteristic is that of a second order low-pass filter with the -3 dB point at approximately 1–3 MHz. The plot can be seen in Figure 3. This plot shows typical behavior with a REF frequency of 50 MHz. There is some amplification in a narrow band just before the roll-off (gain is greater than 0 dB) as is evidenced by the plot. This means that jitter components that fall within this range will be amplified as they pass through RoboClock. This is the reason that it is not recommended to connect more than two RoboClocks in series. Any input jitter at the peaking frequency will be amplified as it passes through the cascaded devices.

Although this problem is evident, the recommended limit of 2 series connected RoboClocks is extremely conservative. The band of jitter amplification changes with temperature and process variation and eventually will result in a lower cascaded multiplication than the peak gain would predict. Thus, in real applications, jitter amplification seldom reaches a point that output jitter causes the system to not function correctly. Also, this type of jitter is not necessarily a problem except between systems served by multiple RoboClocks.

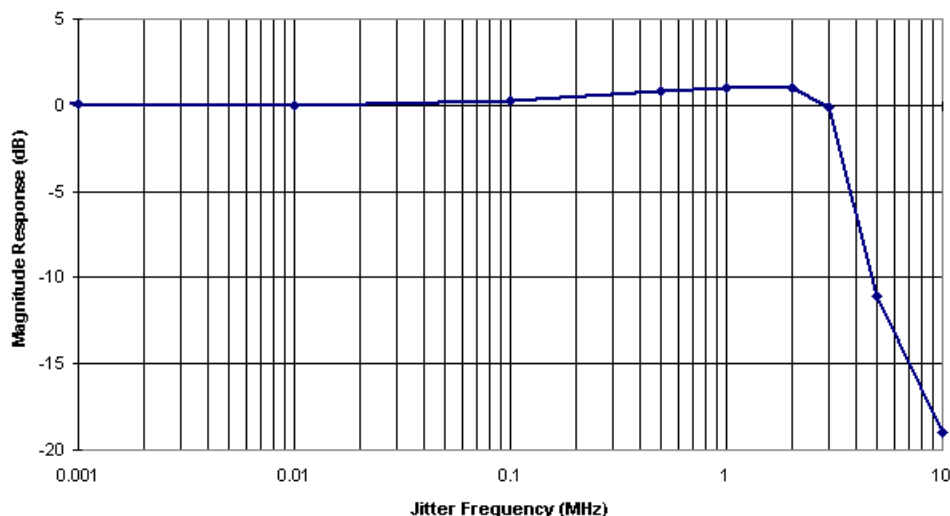


Figure 3. Jitter Transfer Characteristics for RoboClock

6. What are the required voltage levels of a three level input? How do you model a three-level input?

The voltage levels are V_{IHH} , V_{IMM} , and V_{ILL} on the data sheet. For every part in the RoboClock family, except the CY7B991V and CY7B9911V, V_{IHH} is between $V_{CC} - 1V$ and V_{CC} . V_{IMM} is between $V_{CC}/2 - 500\text{ mV}$ and $V_{CC}/2 + 500\text{ mV}$. V_{ILL} is between $0V$ and $1V$. The input left floating will be held within the V_{IMM} range. The ranges for the CY7B991V/11V are from $0.87 \cdot V_{CC}$ to V_{CC} for V_{IHH} , from $0.47 \cdot V_{CC}$ to $0.53 \cdot V_{CC}$ for V_{IMM} , and $0.0V$ to $0.13 \cdot V_{CC}$ for V_{ILL} . These values guarantee that the correct value will be detected. The actual thresholds (high threshold = V_{THH} , low threshold = V_{THL}) will be between the specified ranges, as shown in Figure 4.

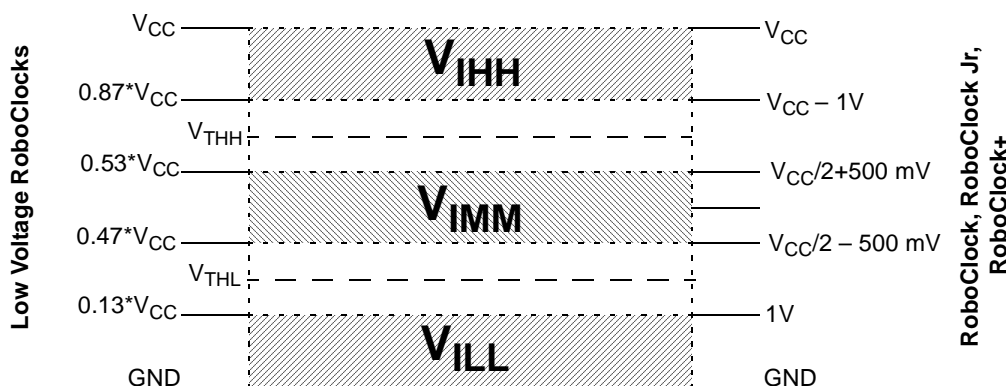


Figure 4. Voltage Levels for Three-Level Inputs

The three-level inputs of the RoboClock family (excluding the CY7B991V/11V) can be modeled by a pull-up and pull-down resistor. The internal resistor values for the three-level inputs are approximately a 25-k Ω pull-up and 25-k Ω pull-down. This is shown in Figure 5. The corresponding I-V curve trace of the three-level input (with $V_{CC}=5.0V$ applied to the part) can be seen in Figure 6. Figure 7 is the same I-V curve trace with the vertical scale zoomed out. The large change in input current at approximately 5.7V and $-0.6V$ are due to the ESD diodes becoming forward biased.

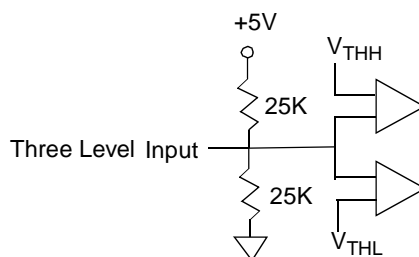


Figure 5. Internal Pull-Up and Pull-Down Resistors of a Three-Level RoboClock Input with Threshold Detection

7. What is the phase relationship between a /2 and /4 output?

They are negative (falling) edge aligned. In Figure 8, the falling edge of the divide by four output (3Q1), is aligned with the falling edge of the divide by two output (4Q1). By having the falling edges of the /2 and /4 clocks aligned, the rising edges are spaced farther in time. If it is assumed that most logic is rising edge triggered, this makes the design more robust to jitter, skew problems, and loading effects. This trade-off is important because the divided outputs are not skewable.

8. What models are available for RoboClock?

There are HSPICE and IBIS models available on the Cypress Semiconductor website (<http://www.cypress.com>).

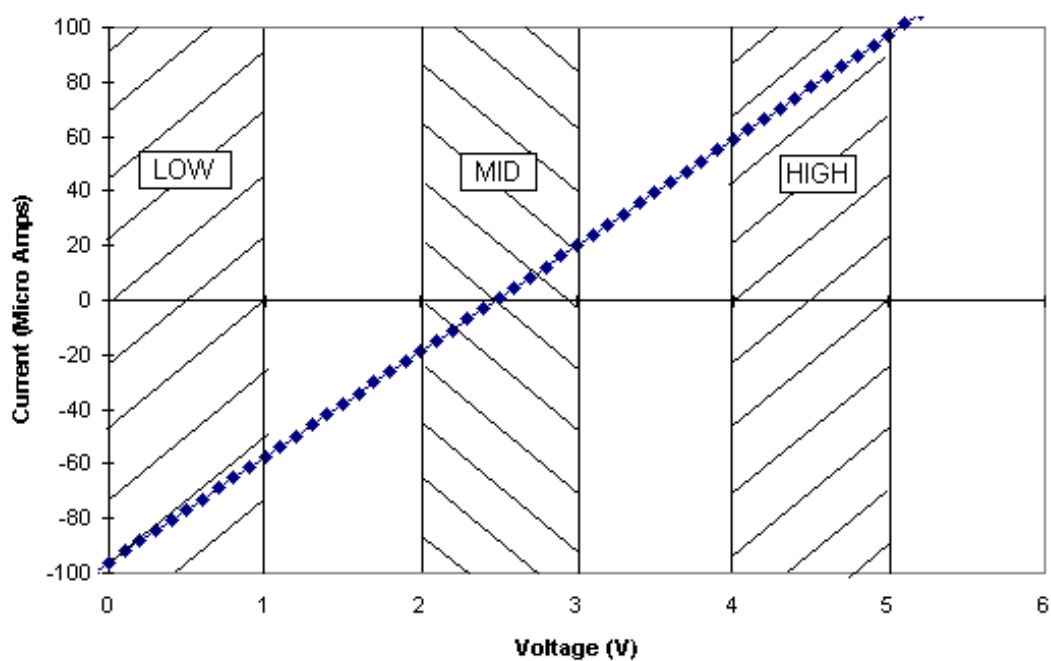


Figure 6. I-V Curve of a Three-Level RoboClock Input (Zoomed In)

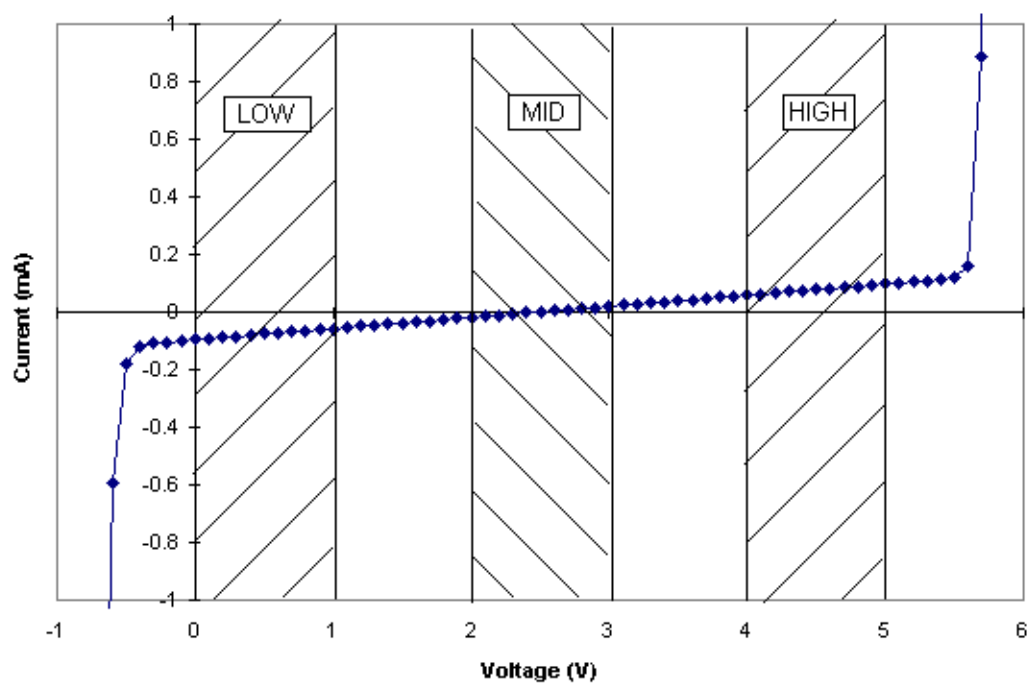


Figure 7. I-V Curve of a Three-Level RoboClock Input

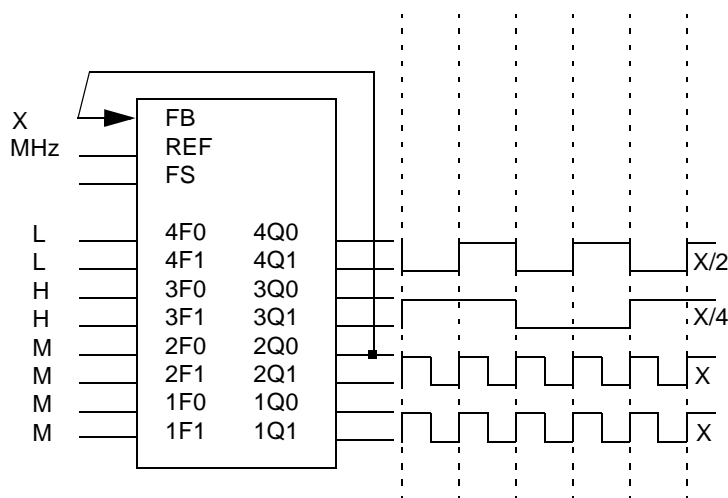


Figure 8. Frequency Divider Example

The Logic Modeling division of Synopsys also offers a wide variety of standard logic models that run on various simulation platforms. These models (cy7b991-XX and cy7b992-XX) accurately depict the functionality of RoboClock. They can be reached at (800) 346-6335 or at their web site:

<http://www.synopsys.com/products/lm/modelDir.html>.

9. How slow can REF go in TEST mode?

There is no lower limit for the REF frequency in TEST mode. This is because in TEST mode the internal PLL is bypassed and the input levels supplied to REF directly control the outputs. The input signal applied to REF will be seen at the outputs with approximately a 15- to 80-ns delay. This delay can be roughly changed by using the TEST and FS level inputs. The outputs will still function according to the function select pins. For a more in depth explanation see the, "RoboClock Family Test Mode" application note. It is available in the Cypress Applications Handbook or off the Cypress Semiconductor website (<http://www.cypress.com>).

10. What effect does slow rise and fall times on the REF input have on RoboClock operation?

A slow rise time affects the apparent t_{PD} , which is the propagation delay (REF rise to FB rise). t_{PD} is measured at an arbitrary but standard 1.5V (CY7B991/10/1V/11V) or $V_{CC}/2$ (CY7B992/20). The actual threshold voltage (V_{TH}) of REF and FB will vary around 1.5V ($0.8V < V_{TH} < 2.0V$ for the CY7B991/10/1V/11V and $1.35V < V_{TH} < V_{CC} - 1.35V$ for the CY7B992/20) depending upon V_{CC} , temperature and process variation. This change in V_{TH} will affect t_{PD} . For example, if input ramp rate is approximately 1 V/ns then 100 mV variation in V_{TH} will change the apparent t_{PD} of the REF and FB input gate by approximately 100 ps. This is normally not a problem, since both FB and REF are threshold matched and are driven by similar edge rates.

If REF ramp rate is much longer than FB, then this "apparent" t_{PD} variation will show up as increased (or decreased) t_{PD} through the RoboClock. Actually (disregarding the minimal effect of edge rate on V_{TH}) the t_{PD} does not change. Only the measurement changes. The propagation delay from the time REF begins to rise, until the time when the output begins to rise, will look like it is increasing with a slower REF rise rate or with increasing REF V_{TH} .

Another possible effect of slow rise and fall times could be introduced jitter. This is due to the increased amount of time that the input is near the threshold voltage. At threshold, the input buffer is much more sensitive to variations and noise.

11. Are there any power-up conditions that cause the part to misbehave?

Yes, there are. This is mentioned in NOTE 3 of the CY7B991/992 data sheet. It states, "When the FS pin is selected HIGH, the REF input must not transition upon power-up until V_{CC} has reached 4.3V". This figure reduces to 2.8V for the low-voltage parts. As the power supply ramps-up, the PLL "wakes-up" before the output buffers. Since the output buffers are not yet functional, there are no transitions on the FB. The PLL "thinks" that it is not running fast enough, so it speeds up, eventually reaching its maximum allowable rate as dictated by the FS pin. Finally, V_{CC} reaches the level where the output buffers become functional. When the FS pin is HIGH, it is possible for the internal VCO to run faster than the outputs can follow (only undivided outputs can exhibit this behavior). Although the outputs are functional, they still can not provide the proper transi-

tions on the FB and thus, the PLL still “thinks” that it is running too slow. The end result is that the VCO locks up at its maximum rate and stays there with the outputs not able to provide the proper transitions.

This condition is not an issue if the RoboClock is operating with the FS pin in the LOW or MID position, or if a divided output is implemented as the feedback. If these conditions are not met then there are a few methods to ensure that this situation does not occur.

1. Assure that REF is stable (no transitions) until V_{CC} reaches 4.3V (point where the output buffers come on. This is 2.8V for the LV parts).
2. Have the part power up in TEST mode (PLL bypassed with mode in MID position).
3. Hold FS pin in LOW or MID (so that PLL will not ramp up to point that outputs can not follow) until V_{CC} is above 4.3V (2.8V for the LV parts).

One way to manage the FS pin is to connect it to a power-on reset. This will ensure that it is LOW until RoboClock has power. If the power-on reset line is 5V CMOS, then it can be connected directly to the FS pin. If it is TTL then it may not be able to drive the FS pin to its HIGH state (see question 6). It may be necessary to use a resistor network to get the proper voltage levels on the FS pin. The implementation may look like *Figure 9*.

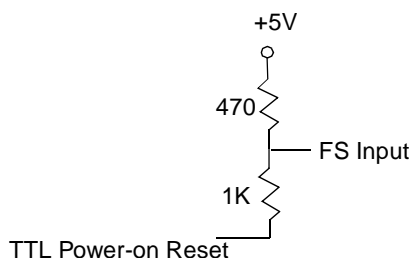


Figure 9. FS Management Using TTL Power-on Reset

Another way to manage the FS pin is by using an RC time constant on the FS pin to make it ramp slower than V_{CC} , holding FS in the LOW or MID state until V_{CC} reaches 4.3V(2.8V for the LV parts) by using a pull-up R and pull-down C. The values of R and C can be determined by the following:

If it takes t seconds for the V_{CC} ramp, then you can find the RC value with the following equation:

$$V_{IMM} \max = V_{CC} (1 - e^{(-t/RC)})$$

$V_{IMM} \max$ = maximum voltage for a MID on the FS pin. From the data sheet, this is $V_{CC}/2+500$ mV. Choose your R and C values so the product equals the calculated RC value. For example, $V_{CC}=5.0V$, and it takes 1 ms for the V_{CC} ramp ($t=1$ ms). R should always be chosen so that it is less than 2.5 k Ω . Then C should be approximately 0.8 mF.

12. What is the output buffer current and output buffer power per output pair?

These specs (minimum and maximum values) are listed in the CY7B991/2 data sheet. They are I_{CCN} and PD respectively. The total output current per output pair (RoboClock has 4 pairs total) can be approximated by the following expression that includes device current plus load current (expressed in mA):

CY7B991/10/1V/11V:

$$I_{CCN} = [(4+0.11F) + (((835-3F)/Z) + (0.0022FC))N] * 1.1$$

CY7B992/20:

$$I_{CCN} = [(3.5+0.17F) + (((1160-2.8F)/Z) + (0.0025FC))N] * 1.1$$

The total power dissipation per output pair can be approximated by the following expression that includes device power dissipation plus power dissipation due to the load circuit (expressed in mW):

CY7B991/10/1V/11V:

$$PD = [(22+0.61F) + (((1550-2.7F)/Z) + (0.0125FC))N] * 1.1$$

CY7B992/20

$$PD = [(19.25 + 0.94F) + (((700 + 6F)/Z) + (0.017FC))N] * 1.1$$

where

F=frequency in MHz

C=capacitive load in pF

Z=line impedance in Ohms

N=number of loaded outputs: 0,1 or 2

FC=F*C

For example, when using a CY7B991 with F=40 MHz, C=30 pF, Z=50Ω, and N=1 (one output loaded, the other floating), the ICCN and PD are calculated as follows:

$I_{CCN} =$

$$[(4 + 0.11 * 40) + (((835 - 3 * 40)/50) + (0.0022 * 40 * 30))] * 1.1$$

$I_{CCN} = 27.87$ mA for this specific output pair

PD=

$$[(22 + 0.61 * 40) + (((1550 - 2.7 * 40)/50) + (0.0125 * 40 * 30))] * 1.1$$

PD=99.264 mW for this specific output pair

13. What do all the different skew values on the data sheet mean?

Skew is the difference in time between the transitions of a pair of outputs with a fixed time relationship. The skew values apply to the skew between different outputs of the RoboClock identically loaded as specified by the data sheet. The skew depends upon the function of the two outputs and in many cases the function of the rest of the outputs.

The outputs of RoboClock have been carefully designed to control delay and edge rate, in an attempt to minimize skew. Outputs are built as pairs (XQ0 and XQ1) sharing the same drive and power supply. The outputs can also be categorized by their function. The classes are nominal, divided, and inverted. Ideally all edges would occur at 0 ns. However, minor variations in internal delay, output rise and fall delay, adjacent output transition direction, and edge placement (coupling) affect the position of the output transition. The six skew specifications shown in the data sheet attempt to quantify these variations.

For further information on how to use these values to calculate the desired skew, see the application note, "Everything You Need to Know About CY7B991/2 (RoboClock) and the RoboClock Family" on the Cypress Semiconductor home page (<http://www.cypress.com>).

t_{SKEWPR}: Zero Output Matched-Pair Skew

This parameter specifies the maximum amount of skew between two outputs of the same pair (e.g., 1Q1 and 1Q0) when all eight outputs are selected for 0t_U.

t_{SKEW0}: Zero Output Skew (All Outputs)

This parameter specifies the time between the first output edge and the last output edge of all outputs that are selected for 0t_U (even if there are other outputs selected for divide-by or invert functionality but not shifted outputs).

t_{SKEW1}: Output Skew (Rise-Rise, Fall-Fall, Same Class)

This parameter specifies the maximum amount of skew between outputs of the same output class selected for the same output adjustment without restrictions on the placement or function of other outputs. The signals to be compared must be same class and must be rising edge to rising edge, or falling edge to falling edge aligned. The three different output classes are Nominal, Divided and Inverted. Nominal includes all phase variants including 0t_U. Divided includes divide by four and divide by 2 functionality. The Inverted class includes the invert function allowed on 4QX.

t_{SKEW2}: Output Skew (Rise-Fall, Nominal-Inverted, Divided-Divided)

This parameter specifies the amount of output skew between the rising or falling edge of a Nominal output and the opposite edge of an Inverted output. It also applies to opposite edge transitions between Divided outputs.

t_{SKEW3}: Output Skew (Rise-Rise, Fall-Fall, Different Class)

This output skew parameter specifies the maximum same edge transition difference between different class outputs.

t_{SKEW4} : Output Skew (Rise-Fall, Nominal-Divided, Divided-Inverted)

This parameter specifies the maximum opposite edge transition difference between different class outputs.

t_{DEV} or t_{SKEW5} : Device-to-Device Output Skew

In system design, t_{DEV} is the amount of skew between the outputs of two devices operating in the same environment (frequency, temperature, voltage, air flow, etc.). It encompasses the worst case for all output possibilities, and therefore is a very conservative number.

t_{SKEW5} is an outdated parameter that does not incorporate the worst case scenario, and required the addition of the applicable output-output skew value to calculate the actual device-device skew. The correct value to use when calculating skew between any two outputs between two devices is t_{DEV} .

t_{PD} : Propagation Delay (REF Rise to FB Rise)

This is a measure of the misalignment between the REF rise and FB rise. It can be either positive or negative. The typical value is 0.0 ns.

14. What is the difference between t_{ODCV} (Output Duty Cycle Variation) and $t_{\text{PWH}}/t_{\text{PWL}}$?

t_{ODCV} is the deviation of the output from 50% duty cycle measured at 1.5V for CY7B991/10/1V/11V and $V_{\text{CC}}/2$ for CY7B992/20. $t_{\text{PWH}}/t_{\text{PWL}}$ is the deviation measured at the corresponding high and low thresholds (t_{PWH} is measured at 2.0V for CY7B991/10/1V/11V and $0.8V_{\text{CC}}$ for CY7B992/20, t_{PWL} is measured at 0.8V for CY7B991/10/1V/11V and $0.2V_{\text{CC}}$ for CY7B992/20). The differences account for rise and fall time “pulse-narrowing” from the 50% point measurement.

15. I need to estimate the reliability in my design. How many components does it contain?

For complete documentation on the reliability of the RoboClock see the yearly Reliability Report. The most commonly desired reliability information is as follows.

Technology:	BiCMOS
Number of components:	3250
Number of transistors:	2130
Number of gates:	275
Die size:	110 mils x 150 mils
Commercial Theta JC:	28 degrees C / Watt
Commercial Theta JA:	80 degrees C / Watt
Max Junction Temp.:	155 degrees C

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